REC'D 07 AVR. 1999
WIPO PCT

DK 99/128

Kongeriget Danmark

Patent application No.: 0361/98

Date of filing: 13 MAR 1998

Applicant: Frank Uldall Leonhard
Louisevej 13
2800 Lyngby
DK

This is to certify the correctness of the following information:

The attached photocopy is a true copy of the following document:

- The specification, claims and drawings as filed with the application on the filing date indicated above

Patentdirektoratet • Kongeriget Danmark

Erhvervsministeriet
Patentdirektoratet

TAASTRUP 26 MAR 1999

Karin Schlichting
Head Clerk

PRIORITY DOCUMENT
SUBMITTED OR TRANSMITTED IN COMPLIANCE WITH RULE 17.1(a) OR (b)

A SIGNAL PROCESSING METHOD FOR DETERMINATION OF A PARAMETER OF A SYSTEM GENERATING THE SIGNAL

The present invention relates to a method for determination of a parameter of a system generating a signal containing information about the parameter.

The method may be used for identification of sound or speech signals, such as in speech recognition, or for quality measurement of audio products or systems, such as loudspeakers, hearing aids, telecommunication systems, or for quality measurement of acoustic conditions. The method of the present invention may also be used in connection with speech compression and decompression in narrow band telecommunication.

The method may also be used in analysis of mechanical vibrations generated by a manufactured device during operation e.g. for detection of malfunction of the device.

The method may further be used in electrobiology for example for analysis of neuroelectrical signals such as analysis of signals from an electroencephalograph, an electromyograph, etc.

BACKGROUND OF THE INVENTION

Prior art methods of signal processing are based on a short time Fourier transform of signals and it is assumed that the signals are steady state signals.

In steady state analysis the signal is assumed stable in the period the signal is analysed and the steady state spectrum is calculated.

In real life steady state signals do not occur and steady state analysis does not provide sufficient knowledge of phenomena within various scientific and technological fields. Consider for example speech analysis. The human ear has the

ability to simultaneously catch fast sound signals, detect sound frequencies with great accuracy and differentiate between sound signals in complicated sound environments. For instance it is possible to understand what a singer is singing in an accompaniment of musical instruments.

It is assumed that the cochlea in the human ear can be regarded as an infinite number of band-pass filters within the frequency range of the human ear.

The time response f(t) for one band-pass filter due to an excitation can be separated into two components, the transient response, $f_t(t)$, and the steady state response, $f_s(t)$, $f(t)=f_t(t)+f_s(t)$.

Traditional signal processing is based on the steady state response $f_s(t)$, and the transient response $f_t(t)$ is assumed to vanish very fast and to be without importance for the perception, see for example "Principles of Circuit Synthesis", McGraw-Hill 1959, Ernest 5. Kuh and Donald O. Pederson, page 12, lines 9-15, where it is stated that:

"only the forced response is considered while the response due to the initial state of the network is ignored".

Thus, when students are introduced to the world of signal analysis, they learn that the transient response, i.e. the response due to the initial state of the network should be ignored because it vanishes within a very short period of time. Furthermore, it is rather difficult to analyse these transient signals by use of traditional linear methods of analysis.

The ability of the human ear to hear very short sounds and at the same time detect frequencies with great accuracy is in conflict with the traditional filterbased spectrum analysis. The time window (twice the rise time) of a band-pass filter is inversely proportional to the bandwidth, $tw=2/(f_u-f_l)$, where f_l is the lower cut-off frequency and f_u is the upper

cut-off frequency.

Thus, if a rise time of 5 ms is required the consequence is that the frequency resolution is no better than 400 Hz.

As the detection of these transients is in conflict with a high frequency resolution, the detecting by the human ear of these transients must take place in an alternative manner. It has not been examined how the human ear is able to detect these signals, but it might be possible that the cochlea, when no sounds are received, is in a position of rest, where the cochlea will be very broad-banded. When a sound signal is received, the cochlea may start to lock itself to the frequency component or components within the signal. Thus, the cochlea may be broad-banded in its starting position, but if one or more stable frequencies are received the cochlea may lock itself to this frequency or these frequencies with a high accuracy.

Today it is known that the nerve pulses launched from the cochlea are synchronized to the frequency of a tone if the frequency is less than about 1.4 kHz. If the frequency is higher than 1.4 kHz the pulses are launched randomly and less than once per cycle of the frequency.

Signal processing based on filter bank spectrum analysis is disclosed in GB 2213623 which describes a system for phoneme recognition. This system comprises detecting means for detecting transient parts of a voice signal, where the principal object of the transient detection is the detection of a point where the speech spectrum varies most sharply, namely, a peak point. The detection of the peak points is used for a more precise phoneme segmentation. The transient analysis of GB 2213623 is based on a spectrum analysis and the change in the spectrum, which is very much different to the transient analysis of the present invention which is based on a direct transient detection in the time domain.

SUMMARY OF THE INVENTION

The present invention provides an approach which is different in principle from all known methods for processing signals. According to the invention it has for example been found that the signal information relevant to recognition of speech is present in a transient part of the speech signal. Thus, the method of the present invention may involve a separation of the transient part of an auditory signal, a generation of a transient pulse corresponding to the transient part, and analysis of the shape of the pulse. In an auditory signal, the corresponding transient pulse may be repeated with time intervals, and the time interval of these periodic transient pulses is normally also analysed or determined.

In real life, the human ear reacts to energy changes at high frequencies in order to recognise phonemes or sound pictures. But in the present method transient pulses corresponding to the energy changes observed by the ear are extracted at these high frequencies, whereafter the transient pulses preferably are transformed to the low frequency range still maintaining the distinct features of the sound pictures or phonemes. Thus, by using the principles of the invention, it is possible to obtain distinct features within auditory signals by examining the transformed low frequency signals.

The invention relates to the use of the shape of energy changes of a signal for identifying or representing features of the system generating the signal for example in recognition of sound features which can be perceived by an animal ear such as a human ear as representing a distinct sound picture are determined.

The method of the present invention provides an expression for the transient conditions of the auditory signal. The method comprises a band-pass filtration of an auditory signal within the frequency range of the human ear and a detection of a low-pass filtered envelope, which envelope then can be analysed with known methods of signal analysis. The envelope

is an expression of the transient part of the signal.

The method of signal analysis, which should be used when analysing the envelope, and the characteristics of the band-pass filter, which should be selected, will depend on the purpose of the analysis. The purpose may be speech recognition, quality-measurement of audio products or acoustic conditions, and narrow band telecommunication.

The invention also relates to a system for processing a signal to reduce the bandwidth of the signal with substantial retention of the information of the signal. The system may further comprise means for extracting the transient component of the auditory signal, and it may comprise means for detecting an envelope of the transient component.

A signal may be separated into a sum of impulse responses generated by poles and zeroes in the system that has generated the signal, if the time between the excitation pulses are sufficient long compared to the duration of the impulse responses for the system.

In WO 94/25958 it is shown that the envelope of the transient component in a speech signal is very important for its recognition and it is shown that the envelope of the impulse response will contain exponential functions and difference frequencies defined by the impulse response.

A method based on damped sinus functions to extract important features from the envelope signal is described, and examples where the method is used on speech signals shows that the features are important in speech analysis.

Before entering into a more detailed explanation of features of the method of the invention, a few definitions will be given:

In short time analysis the transient component in a signal is a matter of definition. For auditory signals, the idea is to

obtain an expression that gives a response corresponding to the response in the cochlea to an abrupt change in the signal energy. An abrupt change in the signal energy corresponds to the transient component in the auditory signal. Thus, in the present context, the term "transient component" designates any signal corresponding to an abrupt energy change in an auditory signal. The transient component holds the signal information to be analysed and in order to analyse this information the transient component may be transformed to a corresponding transient pulse having a distinct shape. Thus, in the present context, the term "transient pulse" refers to a pulse having a distinct shape and substantially holding the information of the transient component of the auditory signal and thus corresponding to an abrupt change in the energy of the auditory signal. As mentioned above the transient part of a sound signal may be repeated with time intervals and thus, in the present context, the term "periodic" when used in combination with a transient component, response or pulse designates any transient component, response or pulse being repeated with intervals.

The term "shape" designates any arbitrary time-varying function (which is time-limited or not time-limited) and which, within a given time interval T_p has a distinctly different amplitude level in comparison with the amplitude level outside the interval. Thus, T_p is the duration of the shape function when the shape function is time-limited, or the duration of the part of the function which has a distinctly different amplitude level in comparison with the amplitude level outside the time interval.

In order to extract information from the shape of the energy changes, one broad aspect of the invention relates to represent the shape of the energy changes by the short time Laplace transform of a transient pulse of the signal. However, several methods can be applied in order to obtain a transient pulse corresponding to the change in energy, but it is preferred that an envelope detection is being used, where the envelope preferably should be detected from a transient

response of the energy change in the auditory signal.

The energy change representing the distinct sound picture can be a phoneme or vowel or any other sound which gives a sudden energy change in an auditory signal.

It is also an aspect of the invention to provide a method for identifying, in an auditory signal, energy changes which can be perceived by an animal ear such as a human ear as representing a distinct sound picture, the method comprising comparing the shape of energy changes of the signal with predetermined energy change shapes representing distinct sound pictures. For the identification it is preferred that the shape of the energy changes are represented by the shape of a transient pulse of the signal, and it is furthermore preferred that the shape of the transient pulse should be obtained by an envelope detection of a transient response of the energy change in the auditory signal.

The invention also relates to a method for processing a signal so as to reduce the bandwidth of the signal with substantial retention of the information of the signal, comprising extracting a transient part of the signal. The method may further comprise detecting an envelope of the transient part of the signal.

Known methods of processing signals are based on a short time Fourier transform of signals, and it is assumed that the signals are steady state signals.

In steady state analysis the signal is assumed stable in the period the signal is analysed, and the steady state spectrum is calculated.

In WO 94/25958 it is disclosed that transient pulses are important for speech coding and decoding in narrow band communication, for speech recognition and synthesis, and for sound quality in auditory products (i.e. loudspeakers, amplifiers and hearing aids).

An important part of a transient signal is the exponential functions or damping ratios or time constants. The damping ratio is the reason that the impulse response has a finite duration. The fact that the transient signal is important for auditory perception indicates that the response from the hair cells are dependent of the time constants. If this is the case, it is possible that the damping ratios in the response from nerve cells in general are important for the human nerve system.

Transient signals are also important in many other applications, among others signals generated by impacts from defects in rolling bearings and gear boxes.

Based on the transient signal, it is possible to determine the natural time constants and frequencies in the system generating the signal. Further it is possible to determine the excitation pulses of the system.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 shows a time-domain representation of a linear time-invariant system,

Fig. 2 shows the impulse response of a Butterworth low-pass filter of 3. order and a cut-off frequency at 700 Hz,

Fig. 3 shows the response with the filter relaxed for $t<0$ and with a 4000 Hz tone as input at $t \geq 0$,

Fig. 4 shows the s-plane with poles and the zero for $H(\sigma,\omega)$,

Fig. 5 shows $H(\sigma,\omega)$ for ω_1 and ω_2 analysed parallel with the σ axis,

Fig. 6 shows transient characteristics in speech signals,

Figs. 7-12 show processed speech signals, and

Fig. 13 shows a schematic of a filter bank according to the present invention.

DETAILED DESCRIPTION OF THE DRAWING

The importance of the transient part of a signal has been an overlooked phenomenon in signal analysis.

The response of a linear system to either an impulse or a step function is defined by its transient response properties.

The relationship between the input and the output for the linear time-invariant system shown in Fig. 1 can be written as the convolution of the input signal and the impulse response of the system:

$$v_o(t) = \int_{-\infty}^{t} v_i(x)h(t-x)dx \qquad (1)$$

If the system is initially relaxed and the input signal $v_i(t)$ is zero for $t < 0$ then the lower integration limit of Eq. (1) can be replaced with zero. Eq. (1) then shows the important role played by the impulse response in terms of the actual signal processing that is performed by the system. It states that the input signal is weighted or multiplied by the impulse response at every instant in time and, at any specific point in time, the output is the summation or integral of all past weighted inputs.

The impulse response of a real system has a finite duration and the transient response has the same duration. Fig. 2 shows the impulse response of a Butterworth low-pass filter of 3. order and a cut-off frequency at 700 Hz. Fig. 3 shows

the response with the filter relaxed for $t < 0$ and with a 4000 Hz tone as input at $t \geq 0$.

In many processes $v_i(t)$ will be a pulse with a short duration and $v_i(t) \approx 0$ before the next pulse will be generated.

The Laplace transform of a signal $v(t)$ is defined by

$$L(s) = \int_0^\infty v(t) e^{-st} dt \qquad (2)$$

$$= \int_0^\infty v(t) e^{-(\sigma - j\omega)t} dt$$

If $v(t)$ is the impulse response $h(t)$ for a system with 2 complex poles

$$h(t) = e^{-(\sigma_0 + j\omega_0)t} + e^{-(\sigma_0 - j\omega_0)t}, \qquad t \geq 0 \qquad (3)$$

and 0 for $t < 0$ and $s \neq -(\sigma_0 \pm j\omega_0)$.

the Laplace transform is

$$H(s) = \frac{s + \sigma_0}{(s + \sigma_0 + j\omega_0)(s + \sigma_0 - j\omega_0)}$$

or

$$H(\sigma, \omega) = \frac{\sigma + \sigma_0 + j\omega}{(\sigma + \sigma_0 + j(\omega + \omega_0))(\sigma + \sigma_0 + j(\omega - \omega_0))} \qquad (4)$$

From Eq. (4) it is seen that for $(\sigma, \omega) \to (-\sigma_0, \pm\omega_0)$, $H(\sigma, \omega) \to \pm\infty$.

This is a well known phenomenon and a logical consequence of this is as follows:

If the signal analysed is dominated by the impulse response of the system generating the signal, it is possible to determine the natural time constants and frequencies for the system.

Fig. 5 shows a plot of H(σ,ω) for $\omega = \omega_1$ and $\omega = \omega_2$.

Analysing a signal along or parallel with the jω axis will give a frequency profile for a given σ.

Analysing a signal along or parallel with the σ axis will give a time constant profile for a given jω.

If a signal has a time constant profile with significant variations for specific frequencies, the signal is transient dominated. Opposite if the signal does not vary significantly for any frequency, the signal is steady state dominated.

A short time Laplace transform is defined by:

$$L(\sigma,\omega,t) = \int_0^t v_i(t-\lambda)e^{-(\sigma-j\omega)\lambda}d\lambda \qquad (5)$$

in which v_i is the signal, L is the transformed signal, σ is a time constant, and ω is an angular frequency.

It is not possible to calculate the short time Laplace transform in the same way as DFT in the discrete time domain because e^{at} and e^{bt}, a and b reel, are not orthogonal functions for $a \neq b$.

The short time Fourier analysis in the analogue time domain is based on a filter bank method. In this paper an equivalent method will be developed for the Laplace transform.

From Eq.(1) and Eq.(3):

$$v_o(t) = \int_0^t v_i(t-\lambda) e^{-(\sigma-j\omega)\lambda} d\lambda$$

$$+ \int_0^t v_i(t-\lambda) e^{-(\sigma-j\omega)\lambda} d\lambda \qquad (6)$$

$$v_o(t) = V(\sigma,\omega,t) + V^*(\sigma,\omega,t) = u(t) + u^*(t)$$

where $u^*(t)$ is the complex conjugate of $u(t)$ and we have

$$\mathrm{Re}\left[L(\sigma,\omega,t)\right] = \tfrac{1}{2} v_o(t) \qquad (7)$$

From Eq.(6) and Eq.(7) it is seen that filtering the signal $v_i(t)$ by a filter with the impulse response $h(\sigma,\omega,t)$ with 2 complex poles will represent the reel part of the short time $L(\sigma,\omega,t)$ transform.

If we let $v_i(t)$ be equal to the impulse response of a single pole we have

$$u(t) = \int_0^t k e^{-(\sigma_0+j\omega_0)(t-\lambda)} e^{-(\sigma+j\omega)\lambda} d\lambda$$

$$= k e^{-(\sigma_0+j\omega_0)t} \int_0^t e^{(\sigma_0+j\omega_0)\lambda} e^{-(\sigma+j\omega)\lambda} d\lambda \qquad (8)$$

$$= \frac{k(e^{-(\sigma+j\omega)t} - e^{-(\sigma_0+j\omega_0)t})}{(\sigma-\sigma_0) + j(\omega-\omega_0)}$$

and from Eq.(7) we have

$$v_o(t) = -\frac{2k(\sigma-\sigma_0)(e^{-\sigma t}\cos(\omega t) - e^{-\sigma_0 t}\cos(\omega_0 t))}{(\sigma-\sigma_0)^2 + (\omega-\omega_0)^2}$$

$$+\frac{2k(\omega-\omega_0)(e^{-\sigma t}\sin(\omega t) - e^{-\sigma_0 t}\sin(\omega_0 t))}{(\sigma-\sigma_0)^2 + (\omega-\omega_0)^2} \qquad (9a)$$

or

$$\frac{v_o(t)}{2k} = \frac{e^{-\sigma_0 t}((\sigma-\sigma_0)\cos(\omega_0 t) - (\omega-\omega_0)\sin(\omega_0 t))}{(\sigma-\sigma_0)^2 + (\omega-\omega_0)^2}$$

$$\frac{-e^{-\sigma t}((\sigma-\sigma_0)\cos(\omega t) - (\omega-\omega_0)\sin(\omega t))}{(\sigma-\sigma_0)^2 + (\omega-\omega_0)^2} \qquad (9b)$$

Eq. (9) is not defined for $(\sigma,\omega) = (\sigma_0,\omega_0)$ but from (8) we have in this case

$$u(t) = ke^{-(\sigma_0+j\omega_0)t}\int_0^t d\lambda$$

$$= kte^{-(\sigma_0+j\omega_0)t}$$

and

$$v_o(t) = 2kte^{-\sigma_0 t}\cos(\omega_0 t) \qquad (10)$$

and we have $v_o(t) \to 0$ for $t \to \infty$.

Eq. (9) shows that the gain is inversely related to $\sigma - \sigma_0$ and $\omega - \omega_0$, and when (σ_0,ω_0) is far from (σ,ω) and $e^{-\sigma t} - e^{-\sigma_0 t}$ is small, $v_o(t) \approx 0$. For $(\sigma_0,\omega_0) \leftarrow (\sigma,\omega)$ $v_o(t)$ will have Eq. (10) as the limit. It is not immediately to see if Eq. (9) has the maximum energy for $(\sigma_0,\omega_0) \leftarrow (\sigma,\omega)$.

In the DC domain Eq.(9) can be written as

$$v_o(t) = 2k\frac{(e^{-\sigma_0 t} - e^{-\sigma t})}{\sigma - \sigma_0} \qquad (11)$$

The maximum for $v_o(t)$ can be found as follows

$$\frac{dv_o}{dt} = \frac{1}{\sigma - \sigma_0}\left[\sigma e^{-\sigma t} - \sigma_0 e^{-\sigma_0 t}\right] = 0$$

when

$$t_m = \frac{\log(\sigma) - \log(\sigma_0)}{\sigma - \sigma_0} \qquad (12)$$

and Eq.(11) will have the maximum for this value.

It can be shown that $t_m \to \frac{1}{\sigma_0}$ when $\sigma \to \sigma_0$.

When $\sigma \approx \sigma_0$ we will have the approximated maximum with $t = \frac{1}{\sigma_0}$

$$v_o(\tfrac{1}{\sigma_0}) = 2k\frac{(e^{-1} - e^{-\frac{\sigma}{\sigma_0}})}{\sigma - \sigma_0} \qquad (13)$$

From Eq.(13) it can be shown that

$$v_o \to \frac{2ke^{-1}}{\sigma_0} \quad \text{for } \sigma \to \sigma_0$$

In Eq.(11) $e^{-\sigma_0 t}$ represent the signal to be analysed and $e^{-\sigma t}$ the filter. Table 1 shows the result with a filter having σ = 100 s^{-1} and the signal varying from 1 to 10000 s^{-1}

It is not surprising that the convolution acts as a low-pass filter. The important fact is that the exponential function in the DC domain in some way acts as frequencies do in the frequency domain.

In table 1 $v_{o1}(t_m)$ is the result of a convolution where the signal is differentiated. The result is, as expected, a high-pass filter

If we look on Eq.(9a) without exponential functions it can be written as

$$v_0(t) = \frac{2k(\sin(\omega t) - \sin(\omega_0 t))}{\omega - \omega_0} \qquad (14)$$

it is seen that for $\omega \to \infty$ we will have $v_o \to 0$.

σ : 100 s^{-1}			
σ_0	t_m	$v_o(t_m)$	$v_{o1}(t_m)$
s^{-1}	s		
1	0,046516871	0,954548457	0,009545485
10	0,025584279	0,774263683	0,077426368
100	0,010000000	0,367879441	0,367879441
1000	0,002558428	0,077426368	0,774263683
10000	0,000465169	0,009545485	0,954548457

Table 1 $v_o(t_m)$ is given by Eq.(11, 12) and normalised by σ and 2k. $v_{o1}(t_m)$ is a convolution where the signal is differentiated and normalised by 2k.

For $\omega << \omega_0$ we will have

$$v_o \cong \frac{2k(\sin(\omega t) - \sin(\omega_0 t))}{\omega_0} \qquad (15)$$

It can be shown that for $\omega \rightarrow \omega_0$ we will have

$$v_o(t) \rightarrow 2kt\cos(\omega_0 t) \qquad (16)$$

This result is as expected unstable.

In transient analysis only the beginning of the signal is of interest, and if $\omega_0 >> 1$ Eq.(14) will act as a band-pass filter.

Speech processing is based on fast energy pulse generated by the vocal cords or by friction in the articulation channel weighted by the impulse response in the articulation channel. The rise time for the excitation pulses has to be sufficient faster than the rise time of the energy of the impulse response.

The shape of energy pulses are important features in speech. If the time between the pulses is periodical it is voiced speech, and if not it is unvoiced speech. For some phonemes abrupt changes in the energy pulses are important.

From WO 94/25958 it is known that the shape of the energy pulses are important for speech recognition, especially the leading edge. In the following a method to extract features will be developed based on an envelope detection.

The convolution expressed in Eq.(9) can be regarded as a response from 2 poles in the articulation channel excited by an impulse. If $\sigma_0 \approx \sigma$ we have from Eq(9a)

$$v_o(t) \cong \frac{e^{-\sigma t}}{(\omega - \omega_0)}\left(\sin(\omega t) - \sin(\omega_0 t)\right) \qquad (17)$$

The envelope is defined as

$$e(t) = \sqrt{u^2(t) + \hat{u}^2(t)}$$

where

$$\hat{u}(t) = u(t) * \frac{1}{\pi t}$$

is the Hilbert Transform.

The envelope of Eq.(17) is then

$$e_o(t) = \frac{e^{-\sigma t}}{|\omega - \omega_0|}\sqrt{(\sin(\omega t) - \sin(\omega_0 t))^2 + (-\cos(\omega t) + \cos(\omega_0 t))^2}$$

$$= \frac{e^{-\sigma t}}{|\omega - \omega_0|}\sqrt{2(1 - \cos(\omega - \omega_0)t)}$$

$$\cong \frac{\sqrt{2}e^{-\sigma t}}{|\omega - \omega_0|}\left(1 - \tfrac{1}{2}\cos((\omega - \omega_0)t)\right) \qquad (18)$$

The approximation is legal because $|\cos((\omega - \omega_0)t)| \leq 1$

As expected the envelope has a component with the difference frequency of the 2 frequencies.

The conclusion is that we can expect to find damped difference frequencies in the envelope of the transient component.

To detect the damped difference frequencies a filter bank is used. The features might be detected as a convolution between the transient pulse and the impulse response of the filters.

In general form the impulse response can be written as

$$h(t) = ke^{-\lambda t} \sin(f(\lambda)t + \phi)$$

Where $\sigma = \lambda$ and $\omega = f(\lambda)$.

In the following analysis $f(\lambda) = 1.5\lambda$, $k = \omega = 1.5\lambda$, and $\phi = 0$ are selected and we have

$$h(t) = 1.5\lambda e^{-\lambda t} \sin(1.5\lambda t) \qquad (19)$$

By selecting $\omega = 1.5\sigma$ Eq.(19) will act as a band-pass filter with a low Q in relation to the frequencies. Other ratios ω/σ than 1.5 may be selected and it is presently preferred that the ratio (ω/σ) ranges from 0.5 to 2.5. The exponential function gives the advance that it acts like natural time window that ensure that the signal is natural damped. The value of the parameters are selected by studying rise times in important transient pulses and by experiments.

Fig. 6 shows transient characteristics in speech signals. The top figure shows 50 ms of an "a" in "hard key" pronounced by a female.

The second signal is a band-pass filtration of the speech signal. The band-pass filter is a Butterworth filter with 6 poles and a band width from 2150 to 3550 Hz. This frequency band contains important transient pulses in the sensitive frequency interval of the ear.

The third signal is a energy detection of the transient characteristics of the band-pass filtered speech signal. The detection is an envelope detection performed by means of a rectification and a low-pass filtration of the signal. The filter is a Butterworth filter with 3 poles and a cut-off frequency at 700 Hz.

In WO 97/09712 a method for automatically detecting the leading edges is disclosed. The method uses the maximum slope of the leading edge as reference, and the point before the maximum slope where the slope is less than a given threshold (10-20 % of the maximum slope) the leading edge is defined to begin.

The transient (envelope) signal in Fig.(6) has a DC component, which does not contain any information. Therefore it is preferred that the signal is differentiated before it is analysed e.g. by the filter bank shown in Fig. 13.

In Fig. 13, the filters ($h_1(t)$, $h_2(t)$,..., $h_n(t)$) in the filter bank connected between the input and the envelope detectors are band-pass filters having bandwidths corresponding to the bandwidths of the band-pass filters of the cochlea and having centre frequencies ranging from 1400 Hz to 6500 Hz.

The output signals $o_{ij}(p)$ from the filter bank shown in Fig. 13 is calculated by:

$$h_{ij}(p) = 1.5\lambda_m e^{-\lambda_m p}\sin(\lambda_m p)\,, \qquad i=0,1,\ldots,N-1 \quad j=0,1,\ldots,M-1$$

$$h_{ij}(p) = 0\,, \qquad p < 0$$

$$o_{ij}(p) = \sum_{k=0}^{P-1} t'(k)h_m(p-k)\,, \qquad p=0,1,\ldots,P-1$$

$m=0,1,\ldots,M-1$ and M is the number of band-pass filters with a low Q in the filter bank connected between the outputs and the envelope detectors, $p = 0,1,\ldots,P-1$ is the sample number, t′ is the differentiated transient signal, and λ_m is the filter bank parameter and it is normalised by the sampling frequency.

In the analysis M is selected to 10 and $1500 \leq \lambda'_m \leq 12000$ s^{-1}, λ'_m is not normalised. By this we have $1885 \leq \omega_m \leq 18850$ s^{-1} or $300 \leq f_m \leq 3000$ Hz.

This filtering process is not done in the cochlea but in the hair cells or in the nerve system behind the hair cells.

The Figs. 7, 8 ,9, 10, 11, and 12 show the output of the processing of transient signals in the vowels "a", "o", "i" in "hard key" and "soft key" pronounced by a female and a male. Further the figures show plots of maxima of the output signals as a function of the time constant σ of the corresponding filter.

The figures show that maximum curves are very much alike for the same vowels, independent of whether it is pronounced by a female or male.

With a library of templates and a distance measure it is possible to identify the sound picture, and it can be used for speech recognition and narrow band communication.

Thus, according to the invention a method and an apparatus are provided for determination of a parameter of a system generating a signal containing information about the parameter, in which the signal is short time transformed substantially in accordance with

$$L(\sigma,\omega,t) = \int_0^t v_i(t-\lambda)e^{-(\sigma+j\omega)\lambda+\varphi}d\lambda$$

in which v_i is the signal, L is the transformed signal, σ is a time constant, ω is an angular frequency, and φ is a phase, or, in accordance with another transformation which will give rise to an $L'(\sigma,\omega,t)$ which in time intervals within which $L(\sigma,\omega,t)$ is larger than 10% of its maximum value is not more than 50% different from the result given by the short time Laplace transformation.

In narrow band communication the transient pulses have to be identified and coded, and the decoder will contain a library of filters with corresponding transient response. The decoder library could also the transient responses.

The present invention also relates to measurement of mechanical vibrations e.g. when testing devices that generate mechanical energy during operation, such as mechanical devices with moving parts, such as compressors for refrigerators, electric motors, household machines, electric razors, combustion engines, etc, etc.

For example, it is known that measurement of vibration generated or sound emitted by a device during operation can be useful for detection of malfunction of the device. Certain failures may generate sound or vibration of specific characteristics that can be recognised.

The method may also comprise steps of classification for classifying a tested device in accordance with the determined parameters into one class of a set of predefined classes. Each predefined class may be defined by a set of upper and lower limits for specific parameters determined according to the method. A device may then be classified as belonging to a certain class if its corresponding parameter values lie within corresponding upper and lower limits of the class.

Each class may correspond to a specific type of failure of the device. For example, shaft imbalance, wheel imbalance, crookedness, imperfections of teeth in cogs, tight bearing, loose bearings, etc, may cause the device to vibrate in different characteristic ways, whereby a characteristic mechanical vibration or sound is generated for each type of failure. The type of failure of the device may then be detected by comparing determined device parameters with corresponding parameter values of various predetermined classes.

The upper and lower limits of a specific class of devices may be determined by testing a set of devices known to belong to that class. For example, the upper limits may be determined as the average of specific parameter values plus three times the standard deviation. Likewise, the lower limits may be determined as the average of parameter values minus three times the standard deviation.

CLAIMS

1. A method for determination of a parameter of a system generating a signal containing information about the parameter, comprising the step of short time transforming the signal substantially in accordance with

$$L(\sigma,\omega,t) = \int_0^t v_i(t-\lambda)e^{-(\sigma+j\omega)\lambda+\varphi}d\lambda$$

in which v_i is the signal, L is the transformed signal, σ is a time constant, ω is an angular frequency, and φ is a phase.

2. A method according to claim 1, wherein the step of transforming comprises filtering the signal v_i with a filter having a pole at σ + jωt and a pole at σ - jωt.

3. A method according to claim 1 or 2, comprising steps of transforming the signal v_i for a plurality of sets of σ and ω values.

4. A method according to any of the preceding claims, further comprising the step of determining a maximum of at least one transformed signal L(σ,ω,t).

5. A method according to any of the preceding claims, further comprising the step of comparing transformed signals L with corresponding reference signals in order to determine parameters of the system.

6. A method according to any of the preceding claims, further comprising a step of pre-processing the signal before the step of short time transforming, the pre-processing being selected from the group consisting of filtering, rectification, differentiation, integration, and amplification.

7. A method of transmitting a signal containing information of a set of parameters of a system generating the signal, comprising processing the signal according to any of the preceding claims and further comprising the step of transmitting the determined parameter values.

8. A method according to claim 7 further comprising the step of regenerating the signal from the determined and transmitted parameter values.

9. A method of transmitting a signal containing information of a set of parameters of a system generating the signal, comprising processing the signal according to any of the preceding claims and further comprising the steps of

comparing the signal with a library of signals generated for a predetermined set of parameter values by the system,

selecting the library function that constitutes the best match to the signal, and

transmitting an identification signal that identifies the matching library function.

10. A method according to claim 9, further comprising the steps of receiving the identification signal and generating the corresponding library signal.

11. A method of classifying a system according to one or more parameters of the system generating a signal containing information about the one or more parameters, comprising determining the one or more parameters according to any of claims 1-6 and further comprising the step of classifying the system in accordance with the one or more determined parameters into one class of a set of predefined classes defined by predetermined ranges of values of the parameters.

12. A method for communicating an auditory signal, comprising processing the signal by the method according to any of claims 1-6, transmitting the processed signal, and receiving the processed signal by a receiver.

13. A method according to claim 12, wherein, prior to transmission of the processed signal, the signal is coded into a digital representation, and the coded signal is decoded in the receiver so as to reestablish transient pulse shapes perceived by the animal ear such as the human ear as representing the distinct sound pictures of the auditory signal.

14. A method according to claim 13, wherein the digital transmission is performed at a bandwidth of at the most 4000 bits per second.

15. A method according to claim 14, wherein the bandwidth is at the most 2000 bits per second.

16. A method according to claim 15, wherein the bandwidth is in the interval of 800-2000 bits per second.

17. A method according to any of claims 13-16, wherein a second and further pulses in a sequence of identical pulses are represented by a digital value indicating repetition.

18. A method according to any of claims 1-6, comprising filtering the signal v_i in a filter bank comprising a plurality of band-pass filters interconnected in parallel with centre frequencies ranging from 1400 Hz to 6500 Hz, each of which is connected in series with an envelope detector and a filter bank comprising a plurality of low-pass filters interconnected in parallel and having cut-off frequencies ranging from 300 Hz to 3000 Hz and time constants σ ranging from 1500 s^{-1} to 12000 s^{-1}.

19. An apparatus for determination of a parameter of a system generating a signal containing information about the parameter, comprising a processor that is adapted to short time transform the signal substantially in accordance with

$$L(\sigma,\omega,t) = \int_0^t v_i(t-\lambda)e^{-(\sigma+j\omega)\lambda+\varphi}d\lambda$$

in which v_i is the signal, L is the transformed signal, σ is a time constant, ω is an angular frequency, and φ is a phase.

20. An apparatus according to claim 19, wherein the processor comprises a filter for filtering the signal v_i and having a pole at σ + jωt and a pole at σ - jωt.

21. An apparatus according to claim 19 or 20, wherein the processor comprises a plurality of filters for filtering the signal v_i, each filter having a different set of σ and ω values.

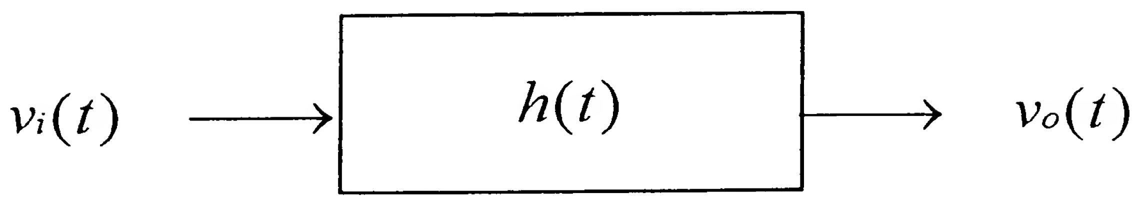


Fig. 1

3. Order, LP, 700 Hz, Butterworth

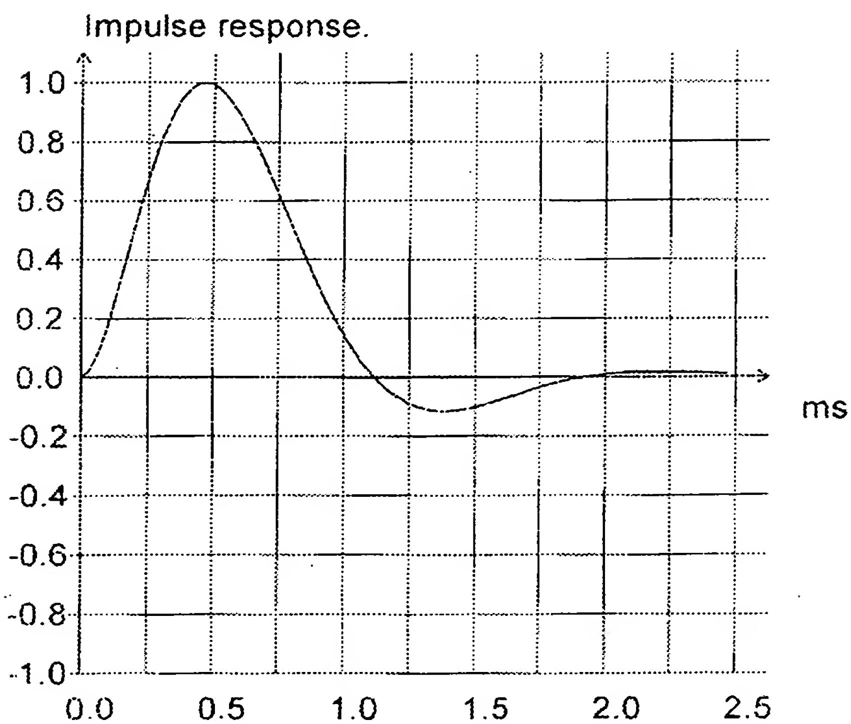


Fig. 2

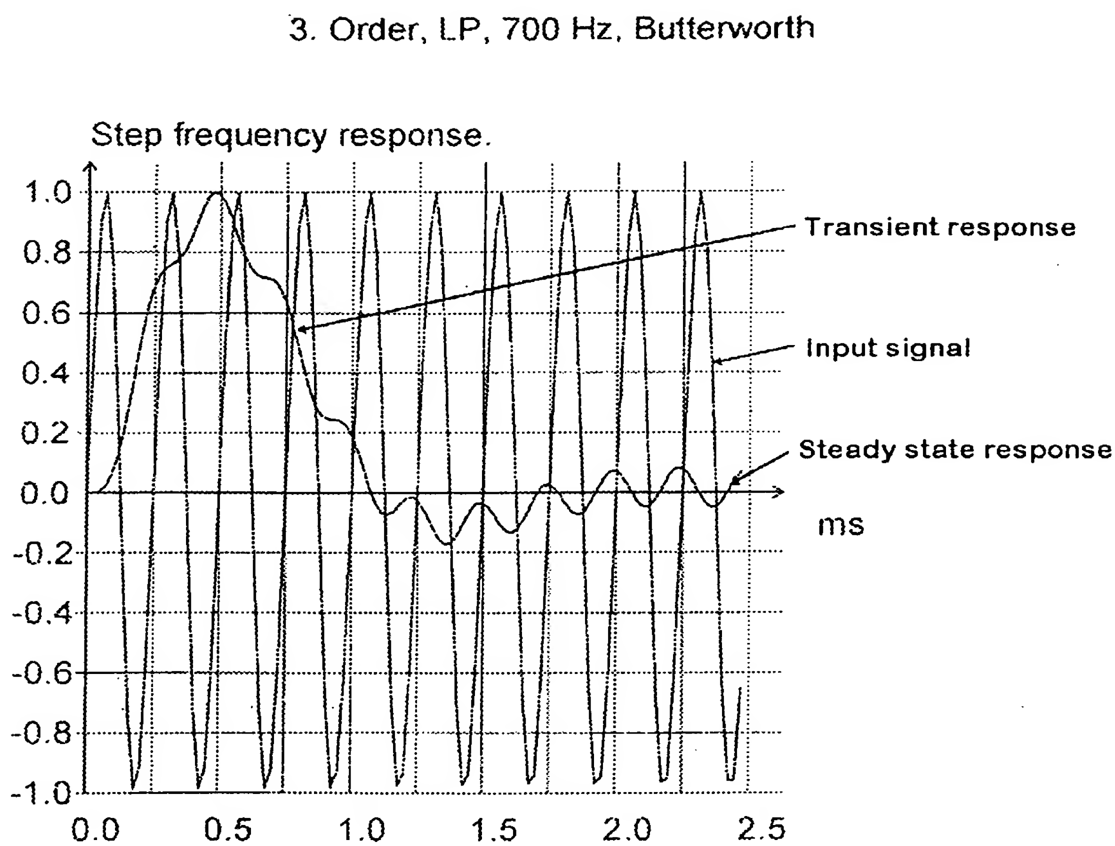

3. Order, LP, 700 Hz, Butterworth
Step frequency response.
1.0
0.8
0.6
0.4
0.2
0.0
-0.2
-0.4
-0.6
-0.8
-1.0
0.0
0.5
1.0
1.5
2.0
2.5
ms
Transient response
Input signal
Steady state response

Fig. 3

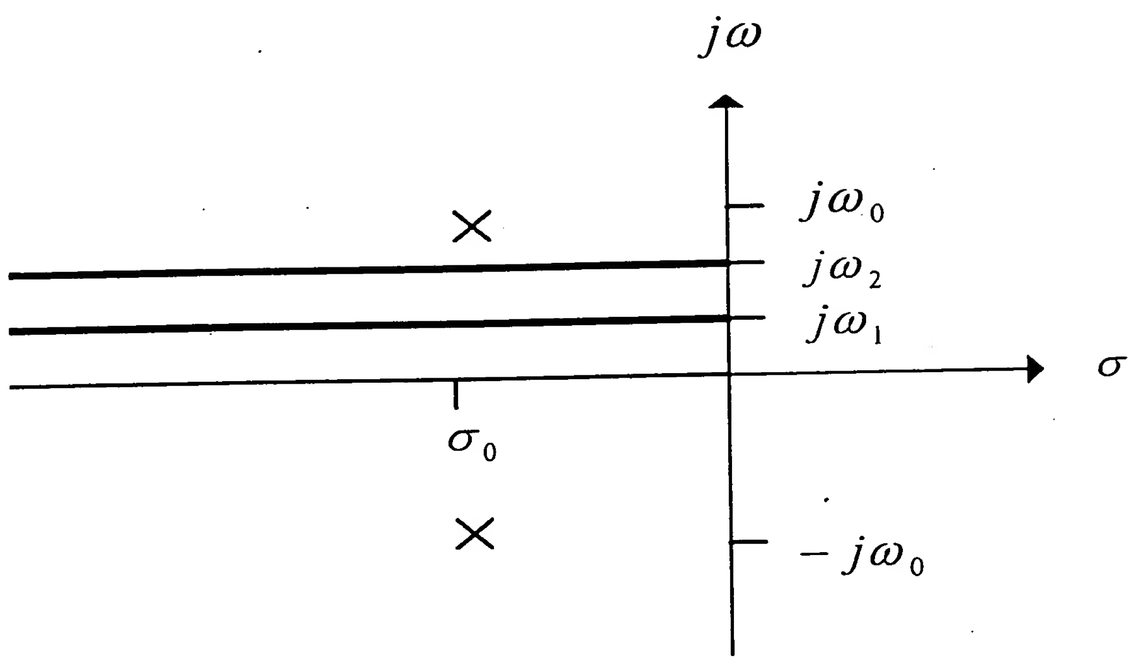


Fig. 4

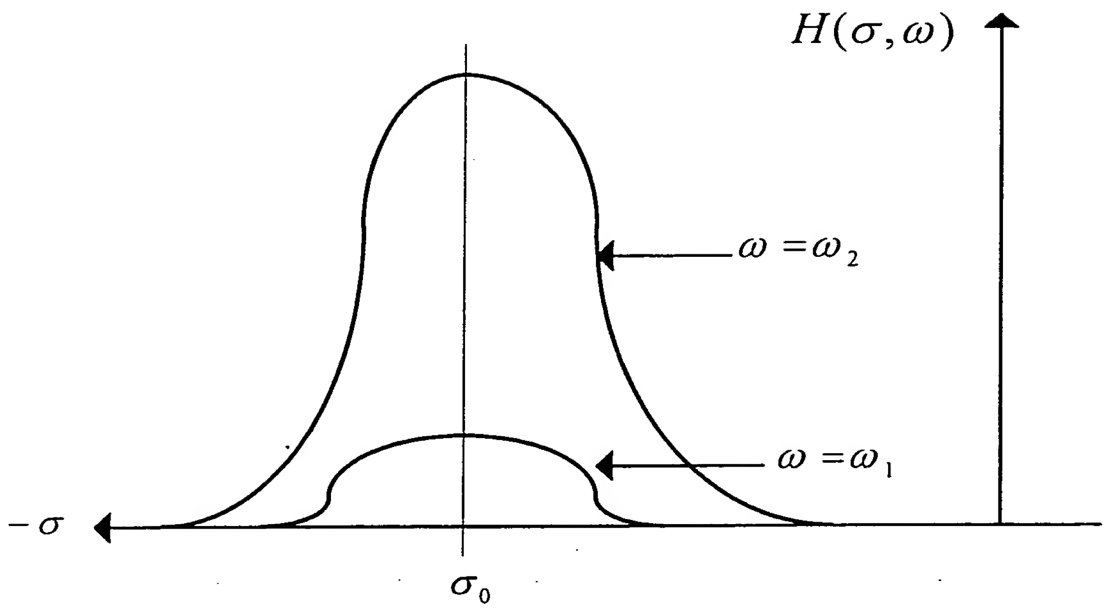
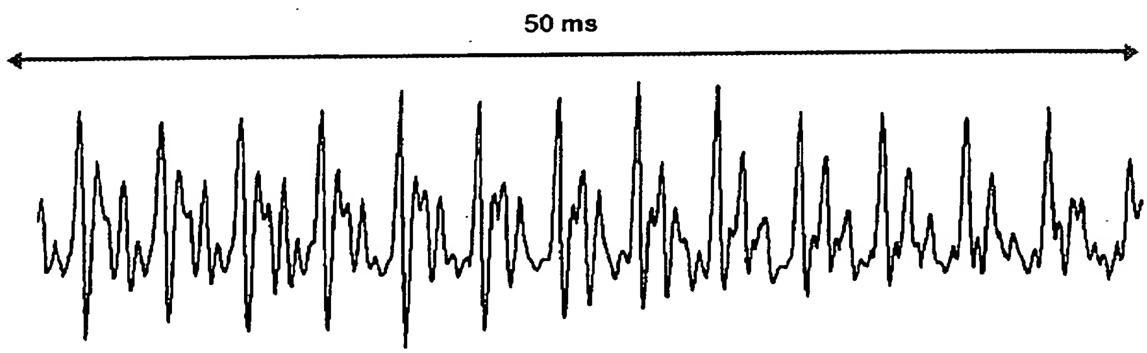
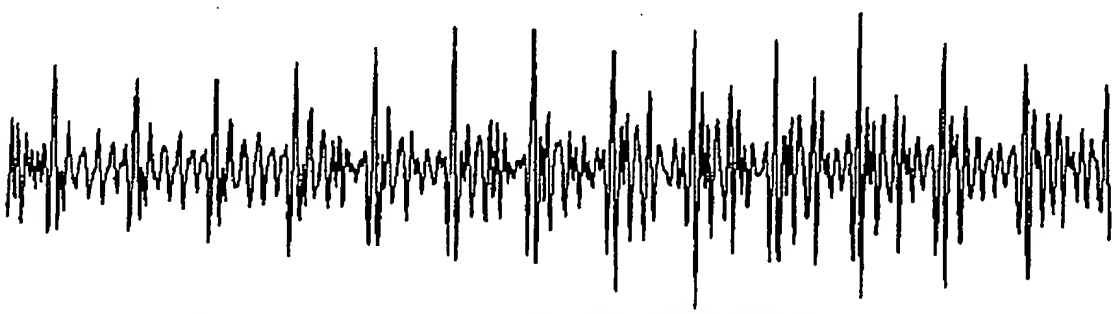


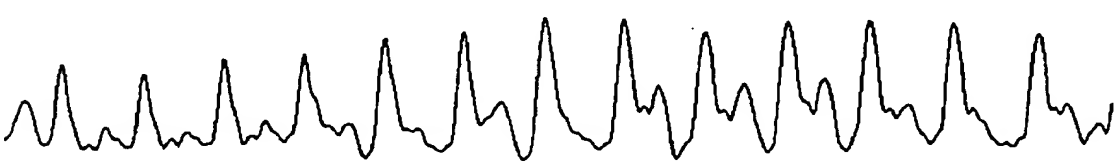
Fig. 5



Speech signal



Transient isolation in the speech signal, band width 2150-3550 Hz



Energy detection of the transient pulses by means of envelop detection, rectified and low pass filtered at 700 Hz

Fig. 6

Sigma	Max	
9250	0.931	0.81633
8500	0.964	0.81633
7750	0.989	0.81633
7000	1.000	0.81633
6250	0.993	0.81633
5500	0.960	0.81633
4750	0.895	0.81633
4000	0.855	0.90703
3250	0.757	0.90703
2500	0.610	0.99773

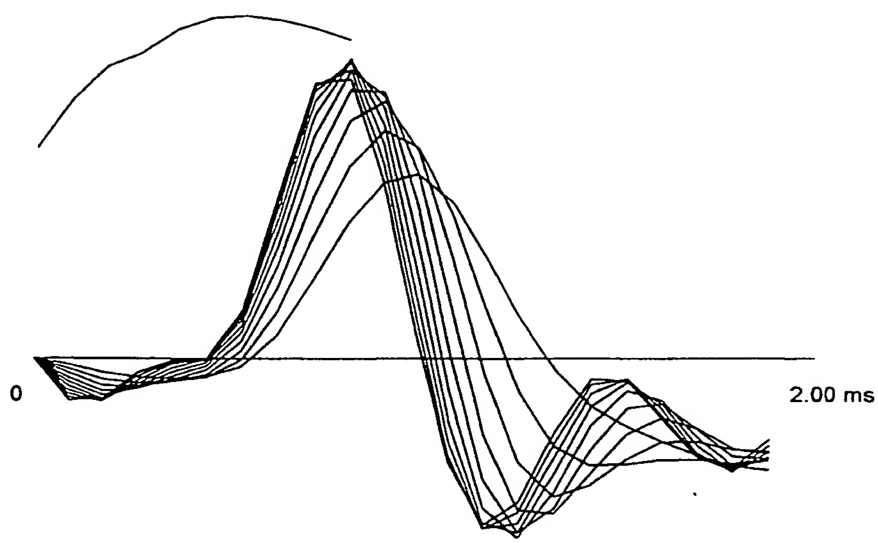


Fig. 7

Sigma	Max	
9250	0.980	0.72562
8500	0.989	0.72562
7750	0.983	0.72562
7000	0.986	0.81633
6250	1.000	0.81633
5500	0.983	0.81633
4750	0.923	0.81633
4000	0.837	0.90703
3250	0.745	0.90703
2500	0.590	0.99773

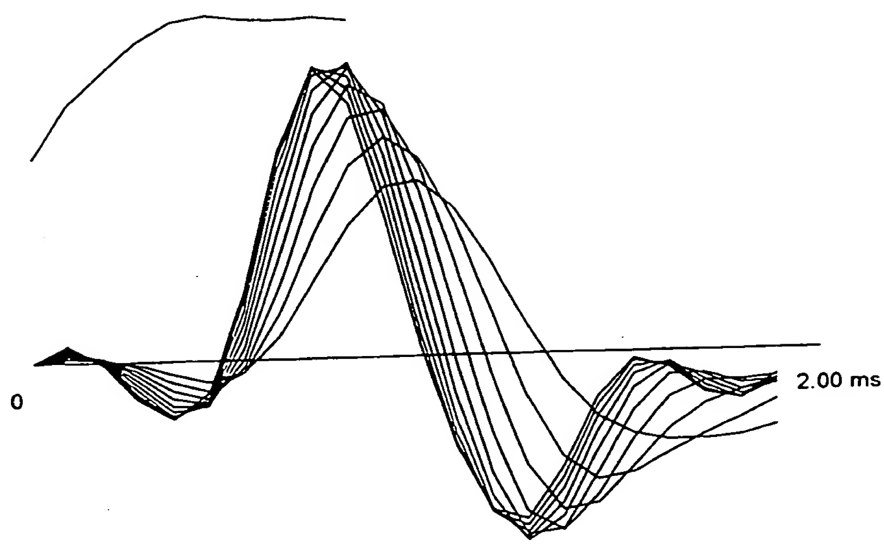


Fig. 8

Sigma	Max	
9250	0.883	0.81633
8500	0.908	0.81633
7750	0.931	0.81633
7000	0.953	0.81633
6250	0.974	0.81633
5500	0.992	0.81633
4750	1.000	0.81633
4000	0.984	0.81633
3250	0.940	0.90703
2500	0.851	0.90703

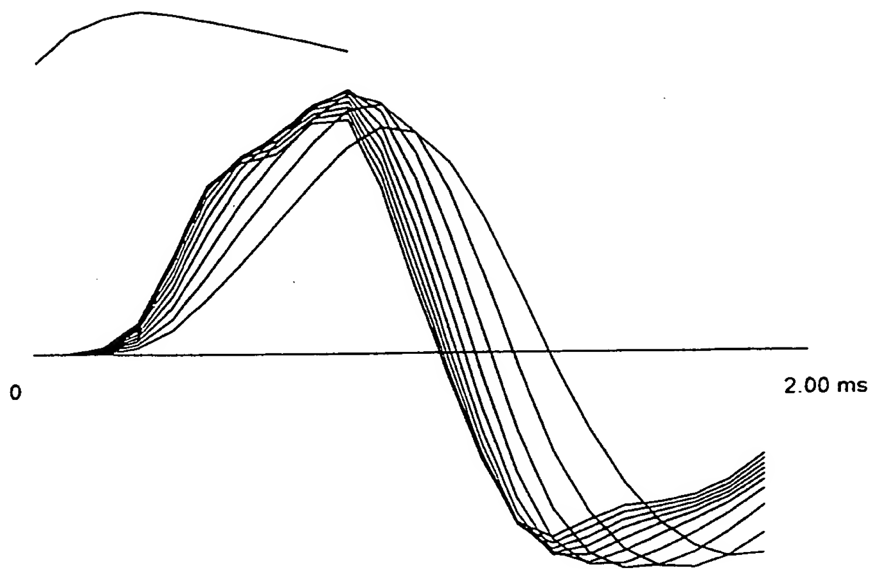


Fig. 9

Sigma	Max	
9250	0.890	0.54422
8500	0.917	0.54422
7750	0.944	0.54422
7000	0.971	0.54422
6250	0.992	0.54422
5500	1.000	0.54422
4750	0.982	0.54422
4000	0.977	0.63492
3250	0.912	0.63492
2500	0.795	0.72562

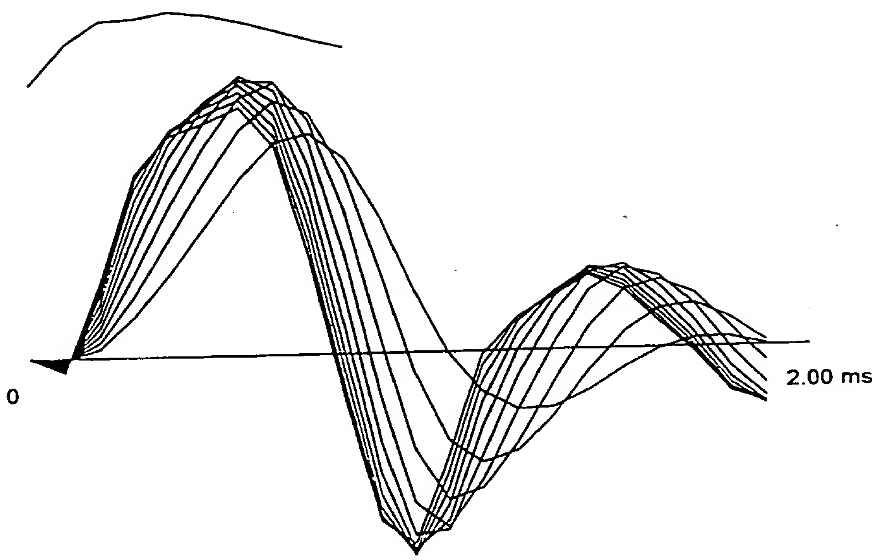


Fig. 10

Sigma	Max	
9250	0.965	0.99773
8500	0.984	0.99773
7750	0.995	0.99773
7000	1.000	0.99773
6250	0.998	0.99773
5500	0.989	0.99773
4750	0.968	0.99773
4000	0.964	1.08844
3250	0.920	1.08844
2500	0.831	1.17914

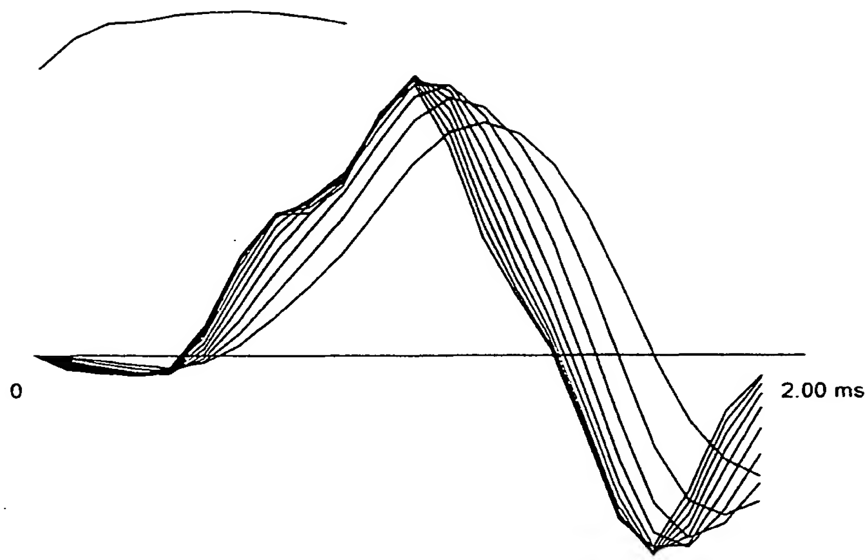


Fig. 11

Sigma	Max	
9250	0.983	0.81633
8500	0.994	0.81633
7750	0.995	0.81633
7000	0.986	0.81633
6250	0.994	0.90703
5500	1.000	0.90703
4750	0.989	0.90703
4000	0.953	0.99773
3250	0.922	0.99773
2500	0.859	1.08844

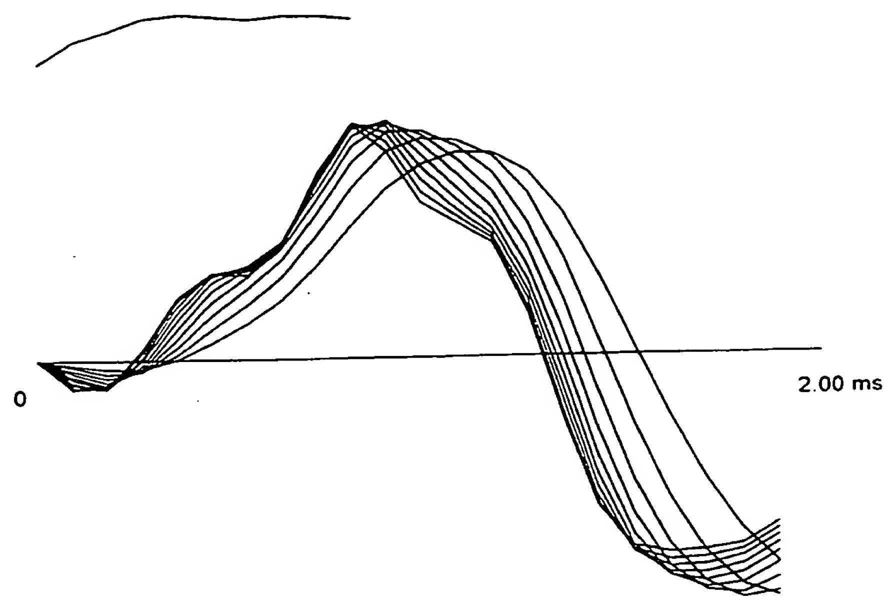
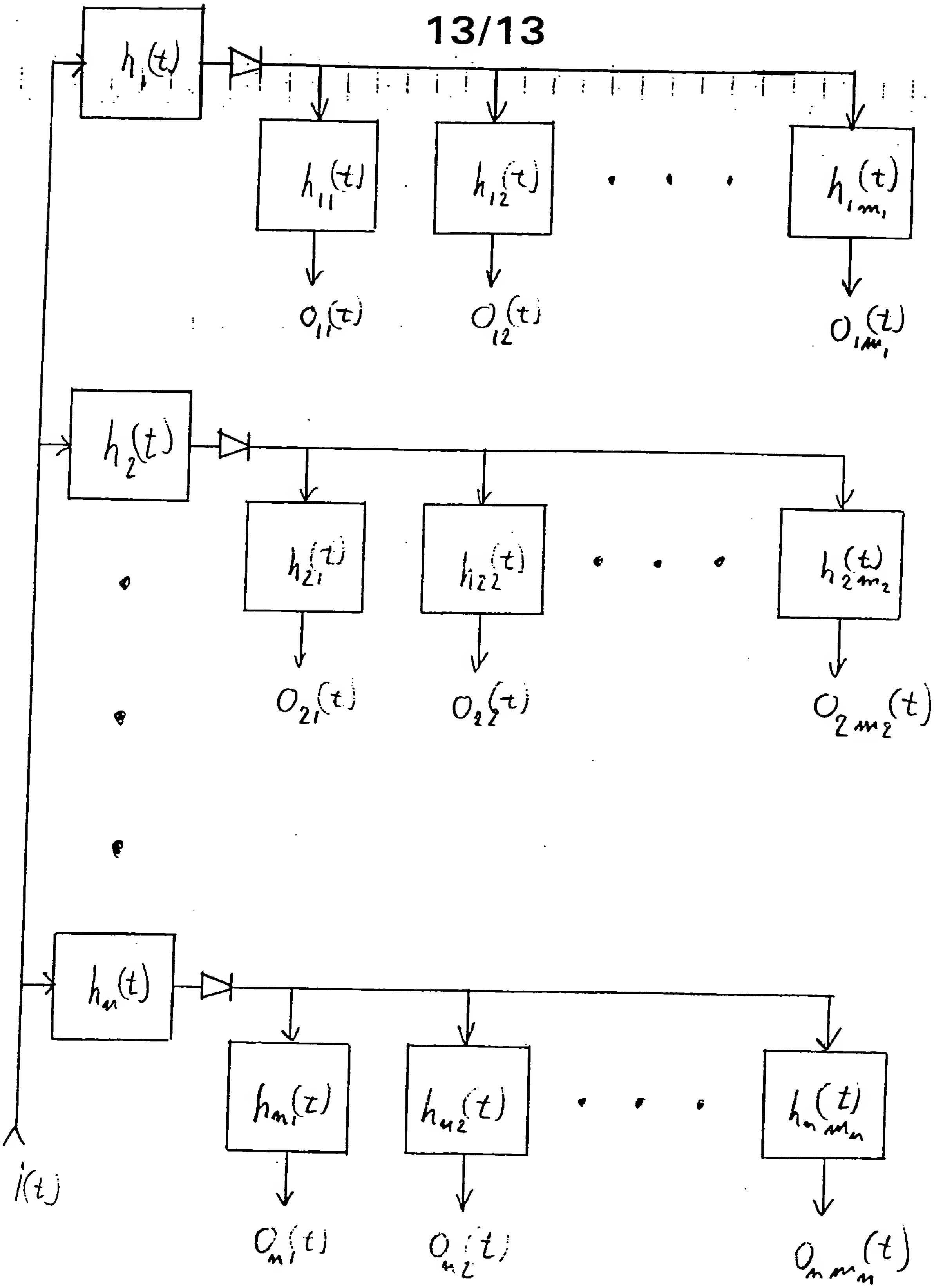


Fig. 12



h1(t)
h11(t)
h12(t)
h1m1(t)
O11(t)
O12(t)
O1m1(t)
h2(t)
h21(t)
h122(t)
h2m2(t)
O21(t)
O22(t)
O2m2(t)
hn(t)
hn1(t)
hn2(t)
hnmn(t)
i(t)
On1(t)
On2(t)
Onmn(t)

Fig. 13